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## Calorimetric investigations on cubic BaTiO<sub>3</sub> and Ba<sub>0.9</sub>Nd<sub>0.1</sub>TiO<sub>3</sub> systems

## R. Babu<sup>a</sup>, R. Kandan<sup>a</sup>, Hrudananda Jena<sup>b</sup>, K.V. Govindan Kutty<sup>b</sup>, K. Nagarajan<sup>a,\*</sup>

<sup>a</sup> Fuel Chemistry Division, Chemistry Group, Indira Gandhi Centre for Atomic Research, Kalpakkam 603 102, Tamilnadu, India <sup>b</sup> Liquid Metals and Structural Chemistry Division, Chemistry Group, Indira Gandhi Centre for Atomic Research, Kalpakkam 603 102, Tamilnadu, India

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## 1. Introduction

Ceramic nuclear waste forms such as synroc, tailored ceramics, TiO<sub>2</sub>-matrix ceramics, glass ceramics and monazite, etc., which are alternative to glass, are under development. The TiO<sub>2</sub>-matrix ceramics, an assemblage of geologically stable titanate minerals and its derivatives have been extensively considered as potential candidates for the immobilization of high level radioactive waste streams, since they are chemically more durable than the silicate assemblage due to their extremely low solubility [1-4]. Titanate ceramic formulations have evolved from the original polyphase assemblage to deal with the wide range of fission products, actinides, process chemicals and also more specific compositions of partitioned fission products or actinides. Alkaline earths and rare earths are the two major groups of fission product elements in the radioactive waste stream. A lanthanide fission product, neodymium, was chosen, in this study, to simulate the behaviour of its transuranium counterpart. The titanates formed by the alkaline earths, such as BaTiO<sub>3</sub> and Ba<sub>1-x</sub>Nd<sub>x</sub>TiO<sub>3</sub> are the probable phases in the waste matrix. In the selection of the nuclear waste forms, the thermodynamic stability of the constituent phases plays a vital role.

Barium titanate is also the most widely used dielectric material for application in multilayer capacitors. Pure and doped barium titanate ceramics also find application as potential candidates for

## ABSTRACT

Drop calorimetric studies were carried out on cubic  $BaTiO_3$  and  $Ba_{0.9}Nd_{0.1}TiO_3$ . Enthalpy increments were measured by inverse drop calorimetric method in the temperature range 573–1523 K using a multidetector high temperature calorimeter. Thermodynamic functions such as heat capacity, entropy, Gibbs energy functions in the temperature range 298–1600 K were computed from the measured enthalpy increments.

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intermediate-temperature fuel cell electrolytes, steam electrolysers, hydrogen and humidity sensors due to their proton conducting nature [5]. Hence the thermodynamic properties of BaTiO<sub>3</sub> and Ba<sub>1-x</sub>Nd<sub>x</sub>TiO<sub>3</sub> are of interest. Heat capacity measurements reported in the literature for BaTiO<sub>3</sub> are limited and data are available only at temperatures below 450 K [6–10]. For the neodymium-doped BaTiO<sub>3</sub>, no data are available. Hence enthalpy increment measurements were carried out on BaTiO<sub>3</sub> and Ba<sub>0.9</sub>Nd<sub>0.1</sub>TiO<sub>3</sub>, having cubic crystal structures, in the temperature range 573–1523 K by drop calorimetry, using a multidetector high temperature drop calorimeter. BaTiO<sub>3</sub> usually crystallizes in the tetragonal system, but in the present case, pristine and Nd-doped BaTiO<sub>3</sub> could be stabilized in the cubic system by employing innovative methods of materials synthesis. The thermodynamic functions of the cubic phases are reported here for the first time.

### 2. Experimental

#### 2.1. Preparation and characterization

BaTiO<sub>3</sub> was prepared in the form of fine powder by gel to crystallite conversion technique and hydrothermal method, as reported in detail elsewhere [11,12]. In both the methods for the preparation BaTiO<sub>3</sub>, the starting materials, Ba(OH)<sub>2</sub> and TiOCl<sub>2</sub> were taken in such a way that the starting stoichiometry of barium and titanium are in the ratio of 1.05:1.0. The hydrated gels of TiO<sub>2</sub>·xH<sub>2</sub>O were precipitated out from dilute aqueous solutions of TiOCl<sub>2</sub>. The gel was washed with boiled distilled water to make it free from chloride and ammonia. The gel was transferred to a Teflon container having a tight lid and weighed amount of Ba(OH)<sub>2</sub>·8H<sub>2</sub>O was added to it. The Teflon container waskept inside an autoclave and heated at 415 K for 4 h. The powders formed were washed thoroughly with boiled distilled water (Co<sub>2</sub>-free) till the powder was free from unreacted Ba(OH)<sub>2</sub>. The oven-dried (373 K) powders were examined by X-ray powder diffraction using CuK<sub>a</sub> radiation, employing a Siemens D-500 powder X-ray diffractometer, in the step scan mode with a step size of 0.02°

<sup>\*</sup> Corresponding author. Tel.: +91 44 27480500x24289; fax: +91 44 27480065. *E-mail address:* knag@igcar.gov.in (K. Nagarajan).

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**Fig. 1.** XRD patterns of pure and Nd-doped BaTiO<sub>3</sub>: (a) and (c) As-prepared samples; (b) and (d) after enthalpy increment measurements.

 $2\theta$ /s and a counting time of 2 s per step. A similar procedure was adopted for the preparation and characterization of Ba<sub>0.9</sub>Nd<sub>0.1</sub>TiO<sub>3</sub>. BaTiO<sub>3</sub> and Ba<sub>0.9</sub>Nd<sub>0.1</sub>TiO<sub>3</sub> synthesized by hydrothermal and gel to crystallite conversion methods were seen to be single phase materials with cubic symmetry (a = 4.03 ± 0.01 Å for Ba<sub>0.9</sub>Nd<sub>0.1</sub>TiO<sub>3</sub>) as revealed by XRD. The XRD patterns of the as-prepared samples and that of the samples after calorimetric measurements are shown in Fig. 1, and there is no phase transformation in the temperature range of measurement.

#### 2.2. Multi-detector high temperature calorimeter

The enthalpy increments of the titanates were determined by drop calorimetry using SETARAM multi-detector high temperature calorimeter (MHTC-96). The calorimetric detector is a thermopile comprising 28 thermocouples embedded on the inner side of an alumina tube in which the sample crucible and an empty reference crucible are positioned one above the other. In the thermopile detector, the thermocouples are positioned at heights surrounding the outer surfaces of the crucibles so that an integrated heat exchange between the two crucibles is obtained at the output signal. In the present study, a detector, made up of Pt-30%Rh/Pt-10% thermocouples was employed. The detector is centered in a gas-tight alumina muffle placed in the furnace heated by a single graphite resistance element. All measurements were performed in ultra high pure argon atmosphere.

#### 2.3. Enthalpy increment measurements

In a typical experiment, carried out at a constant temperature four or five titanate sample pellets and an equal number of  $\alpha$ -alumina reference (SRM 720) pellets each weighing about 150–200 mg, were dropped one after the other from the specimen chamber maintained at the ambient temperature into the sample crucible kept in

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<i>T</i> (K)	$H_T - H_{298}$ (kJ mol <sup>-1</sup> )			
	Experimental	Calculated from Eq. (1)		
573	34.901	32.321		
623	39.993	38.697		
673	45.455	45.157		
723	55.112	51.690		
773	60.004	58.289		
823	64.850	64.946		
873	70.128	71.657		
923	76.920	78.418		
973	86.050	85.226		
1023	92.136	92.078		
1073	97.846	98.973		
1123	106.609	105.909		
1173	112.103	112.884		
1223	116.386	119.898		
1273	123.899	126.949		
1323	136.170	134.037		
1373	139.236	141.161		
1423	153.076	148.320		

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Enthalpy	increments	of Ba <sub>0.9</sub>	$Nd_{0.1}TiO_3$ .

<i>T</i> (K)	$H_T - H_{298}$ (kJ mol <sup>-1</sup> )	$H_T - H_{298}  (\text{kJ}  \text{mol}^{-1})$		
	Experimental	Calculated from Eq. (2)		
573	37.330	32.607		
623	42.661	39.054		
673	47.347	45.594		
723	54.390	52.215		
773	60.404	58.909		
823	67.318	65.671		
873	71.782	72.494		
923	76.910	79.376		
973	87.553	86.313		
1023	92.099	93.304		
1073	97.035	100.346		
1123	103.633	107.438		
1173	114.355	114.579		
1223	121.611	121.766		
1273	128.896	129.000		
1323	136.211	136.280		
1373	143.556	143.605		
1423	150.930	150.973		
1473	159.904	158.386		
1523	167.287	165.842		

the calorimeter maintained at a constant temperature *T*. From the resultant heat flow signals corresponding to the  $\alpha$ -alumina reference ( $Q_R$ ) and the titanate sample ( $Q_S$ ), the enthalpy increments of the titanate samples ( $H_T - H_{298}$ )<sub>S</sub> were computed using the known enthalpy increment values of  $\alpha$ -alumina reference ( $H_T - H_{298}$ )<sub>R</sub> from the literature [13] and the following expression:

$$(H_{T} - H_{298})_{S} = \frac{\int Q_{S} dt}{\int Q_{R} dt} \cdot \frac{M_{S}}{m_{S}} \cdot \frac{m_{R}}{M_{R}} \cdot (H_{T} - H_{298})_{F}$$

where  $M_R$  and  $m_R$  are the molar mass and mass of the  $\alpha$ -alumina reference material and  $M_S$  and  $m_S$  are the molar mass and mass of the titanate sample. The mean of the five heat flow values for the standard and that for the sample were used to compute the enthalpy increment at that temperature, *T*. Further, four or five measurements were carried out for a given temperature and the mean value of the enthalpy increments from these runs at temperature, *T* were used for fitting.

#### 3. Results and discussion

The accuracy of the enthalpy increments from our measurements had been determined to be 2-4%. Enthalpy increments of BaTiO<sub>3</sub> and Ba<sub>0.9</sub>Nd<sub>0.1</sub>TiO<sub>3</sub> were measured in the temperature ranges of 573-1423 K and 573-1523 K, respectively. They were fitted to polynomial functions in temperature by the least squares method using the following two constraints: (i)  $(H_T - H_{298}) = 0$  at 298 K; (ii) the derivative of the function at 298 K is equal to the value of heat capacity at 298 K. The C<sub>p,298</sub> values for the BaTiO<sub>3</sub> and  $Ba_{0.9}Nd_{0.1}TiO_3$  (which were estimated from  $C_{p,298}^0$  of its constituent oxides from the literature [14] by invoking molar additivity rule to be 101.87 and 102.76 J K<sup>-1</sup> mol<sup>-1</sup>, respectively). Similarly the  $S_{298}^0$ value of BaTiO<sub>3</sub> and S<sub>298</sub> value of Ba<sub>0.9</sub>Nd<sub>0.1</sub>TiO<sub>3</sub> needed for computing entropy and Gibbs energy functions were also estimated from the entropy values of constituent oxides [14]. However, for the estimation of S<sub>298</sub> value Ba<sub>0.9</sub>Nd<sub>0.1</sub>TiO<sub>3</sub> the contribution of ideal entropy of mixing was taken into consideration. The fit equations thus obtained for BaTiO<sub>3</sub> and Ba<sub>0.9</sub>Nd<sub>0.1</sub>TiO<sub>3</sub> are given below:

BaTiO<sub>3</sub>

$$(H_T - H_{298}) = 127.561T + 6.064 \times 10^{-3}T^2 + 26.052 \times 10^5 T^{-1} - 47,309$$
(1)

Ba<sub>0.9</sub>Nd<sub>0.1</sub>TiO<sub>3</sub>

$$(H_T - H_{298}) = 126.636T + 7.883 \times 10^{-3}T^2 + 25.403 \times 10^5 T^{-1} - 46,978$$
(2)

## Table 3

Thermodynamic functions of BaTiO<sub>3</sub> calculated from Eq. (1).

<i>T</i> (K)	$H_T - H_{298}  (\text{kJ mol}^{-1})$	$C_P$ (J K <sup>-1</sup> mol <sup>-1</sup> )	$S_T (J K^{-1} mol^{-1})$	$-(G_T - H_{298})/T(J K^{-1} mol^{-1})$
298	0	101.87	122.70	122.70
300	0.189	102.25	123.33	122.70
400	11.198	116.13	154.90	126.91
500	23.198	123.20	181.65	135.26
600	35.752	127.60	204.53	144.94
700	48.677	130.73	224.45	154.91
800	61.877	133.19	242.07	164.72
900	75.302	135.26	257.88	174.21
1000	88.921	137.08	272.23	183.30
1100	102.714	138.75	285.37	191.99
1200	116.667	140.31	297.51	200.29
1300	130.772	141.79	308.80	208.21
1400	145.022	143.21	319.36	215.77
1500	159.413	144.60	329.29	223.01
1600	173.940	145.95	338.66	229.95

#### Table 4

Thermodynamic functions of Ba<sub>0.9</sub>Nd<sub>0.1</sub>TiO<sub>3</sub> calculated from Eq. (2).

T (K)	$H_T - H_{298}  (\text{kJ}  \text{mol}^{-1})$	$C_P$ (J K <sup>-1</sup> mol <sup>-1</sup> )	$S_T$ (J K <sup>-1</sup> mol <sup>-1</sup> )	$-(G_T - H_{298})/T (J K^{-1} mol^{-1})$
298	0	102.76	120.72	120.72
300	0.190	103.14	121.36	120.72
400	11.289	117.17	153.19	124.97
500	23.392	124.36	180.17	133.38
600	36.076	129.04	203.28	143.15
700	49.159	132.49	223.41	153.21
800	62.552	135.28	241.32	163.13
900	76.203	137.69	257.40	172.73
1000	90.082	139.86	272.02	181.94
1100	104.170	141.88	285.44	190.74
1200	118.454	143.79	297.87	199.16
1300	132.926	145.63	309.45	207.20
1400	147.578	147.41	320.31	214.90
1500	162.407	149.16	330.54	222.27
1600	177.408	150.87	340.22	229.34

In the above equations, the temperature is expressed in K and the enthalpy increment in J mol<sup>-1</sup>. The standard errors of the fit are 2.7% and 2.4% and the estimates of the standard deviations for the fit are 2438 J mol<sup>-1</sup> and 2339 J mol<sup>-1</sup> for BaTiO<sub>3</sub> and Ba<sub>0.9</sub>Nd<sub>0.1</sub>TiO<sub>3</sub>, respectively. The experimental values of the enthalpy increments of BaTiO<sub>3</sub> and Ba<sub>0.9</sub>Nd<sub>0.1</sub>TiO<sub>3</sub> are given in Tables 1 and 2 along with the calculated values from Eqs. (1) and (2). From the above fit equations, heat capacity, entropy and Gibbs energy function have also been computed which are given in Tables 3 and 4. The measured enthalpy increment values of BaTiO<sub>3</sub> and Ba<sub>0.9</sub>Nd<sub>0.1</sub>TiO<sub>3</sub> are shown in Fig. 2 along with the fit values as well as those computed using molar additivity rule from the enthalpy data of the component oxides from the literature [13]. The values from the fit are within  $\pm 3\%$  of the measured values. Present enthalpy increment data are in agreement within 4% with the mole average values calculated for BaTiO<sub>3</sub> and Ba<sub>0.9</sub>Nd<sub>0.1</sub>TiO<sub>3</sub>. Fig. 3 shows the present heat capacity data for BaTiO<sub>3</sub> and Ba<sub>0.9</sub>Nd<sub>0.1</sub>TiO<sub>3</sub> along with the heat capacity data computed from the literature by using the molar



Fig. 2. Enthalpy increments of pure and Nd-doped BaTiO<sub>3</sub>.



Fig. 3. Heat capacity of pure and Nd-doped BaTiO<sub>3</sub>.

additivity rule. As can be seen from Fig. 3, the present heat capacity data are higher than the mole average values. The deviations are about 4 and 5% for pure  $BaTiO_3$  and  $Ba_{0.9}Nd_{0.1}TiO_3$  at 1000 K and they increase with increase in temperature. The larger deviation at higher temperatures could be due to the contribution of anharmonicity.

## 4. Conclusion

Enthalpy increments of BaTiO<sub>3</sub> and Ba<sub>0.9</sub>Nd<sub>0.1</sub>TiO<sub>3</sub> having cubic crystal structures have been measured in the temperature ranges 573–1523 K for the first time by inverse drop calorimetry. Other thermodynamic functions, namely, heat capacity, entropy and Gibbs energy functions were computed in the temperature range 298–1600 K.

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